Appendix E: Precast R-Value Calculations





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SULATION

The next analysis that was performed was the **Steady State Isothermal Analysis Method #1:**

Using a series-parallel method of calculation, Isothermal Analysis predicts the effects of irregular sized and spaced penetrations through an insulation layer. Individually, steel or concrete have significant effects on the insulation layer and can be predicted with this analysis method.

The Isothermal Analysis by itself has been proven a bit aggressive when figuring the effects of solid concrete sections and therefore has been tempered with U-Value average to account for the restricted conduction zones affected by solid concrete.

The steady state thermal analysis shows the total isothermal R-value for the wall, with the ability to factor in thermal breaks such as metal ties or solid concrete sections.

You will notice in the findings shown in the Isothermal Analysis that the THERMOMASS wall panel has a material R-Value of **R-11.49**. The Isothermal Analysis shows **.90%** thermal loss in this wall panel with the use of fiber composite connectors. The overall material R-Value of the THERMOMASS wall consists of an **R-11.39**.

The competing wall system which consists of 2X4 steel studs (16" oc), 2" XPS insulation, full exterior brick w/ brick ties connected back to the steel studs. Due to the thermal conductivity of the brick ties this assumed R-11.66 wall actually performs at an **R-7.76** (33% reduction).

TOLL FREE: 1.800.232.1748



Steady-State Thermal Analysis by Modified Isothermal Analysis Method

Study Provided For: Penta Career Center - Perrysburg, OH 3"/2"/5" TM vs. 2x4 steel stud 2"XPS & brick (pt 1)



ASSUMPTIONS: All values for extruded insulation based on ASTM C-578 specifications for Type IV - extruded polystyrene insulation @ base temperature of 75°F. -Part 1 of 2 - Value for brick veneer calculated to equal 10 inches of concrete.

This Modified "Isothermal Planes" Method combines Series-Parallel Path Analysis, ASHRAE Handbook - 2001 Fundamentals, Chapter 23 and U-value Average Analysis as validated through CTC/DOE Thermal Study 1999.

CALCULATED RESULTS SUMMARY

	THERMOMASS® SPEC.				PANEL DESIGN #2					
	R-VALUE		LOSS		R-VALUE	% of L		LOSS		
	Assumed	Isothermal	%	Assumed	Isothermal	Modified	To Iso.	To Mod.		
Г	6.49	6.44	0.80%	6.66	4.71	4.71	29.32%	29.32%		
Г	8.99	8.91	0.86%	9.16	6.23	6.23	31.95%	31.95%		
ſ	11.49	11.39	0.90%	11.66	7.76	7.76	33.46%	33.46%		
Г	16.49	16.33	0.94%	16.66	10.81	10.81	35.11%	35.11%		
Г	21.49	21.28	0.96%	21.66	13.86	13.86	36.00%	36.00%		
Г	26.49	26.23	0.98%	26.66	16.91	16.91	36.56%	36.56%		
Γ	31.49	31.18	0.99%	31.66	19.96	19.96	36.94%	36.94%		
Г	36.49	36.13	0.99%	36.66	23.02	23.02	37.21%	37.21%		
ſ	41.49	41.08	1.00%	41.66	26.07	26.07	37.42%	37.42%		

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ULATION

MASS ANALYSIS 1.2

Performance Mass Analysis:

A precast concrete sandwich wall panel system constructed with The THERMOMASS Insulation System maximizes the thermal mass effect of concrete, thereby reducing the heating and cooling loads and providing an R-Value greater than what can be expected by the material alone (R-11.49) or by which code requires.

When utilizing climate data for Perrysburg, OH the proposed 3-in exterior concrete / 2-in extruded polystyrene insulation / 5-in interior concrete THERMOMASS Wall Panel performs at **R-20.64**.

This is determined by taking into account climate data, building orientation, occupancy type, and facility type. ASHRAE/IESNA Standard 90.1-1989: System Performance Criteria is the standard calculation used.

This criteria determines the R-Value performance and the heating and cooling load adjustments for the effects of concrete mass within the building envelope. The results of the analysis are detailed in image to the right.

ASHRAE 90.1-2001 Compliant Building Envelope Performance Study

Study Provided For:

Penta Career Center - Perrysburg, OH

3"/2"/5" THERMOMASS - Edge to edge XPS insulation

SYSTEM PERFORMANCE CRITERIA

The result of the balanced equation comparison of the designed, high-mass concrete wall to the similarly designed, non-mass wall is a relationship of energy performance in Btu's to R-value. Note: The material wall R-value is not altered by the dynamics of the building and the climate. The performance value represented below is a portrayal of energy consumption as a function of insulation performance.

PERFORMANCE STUDY SUMMARY

Th		North	Fast	South	West	STEADY-
¥	000	ING LOAD	FOR DEST	NED WALL		STATE WALL
	WCc	3 003577	2 946804	3 344073	2.766502	D-value:
9	WCt	12.060956	2.5 10001	5.5 11075	2.700002	R-value.
H	Btu Consumption	12 060 956				11.49
≍ I	212 001101101	,,				STEADY-
5	HEAT	STATE WALL				
S	WCh	4.397850	4.244893	3.820091	4.215030	U-value:
I	WCt	16 677863				0.007
ION	Btu Consumption	16.677.863	Note I: Btu's consumed	equals	0.087	
2	TOTAL ESTIMA					
E	WCt	28.739	Wall Criteria results in a zero			
H	Btu Consumption 28,738,819 value for final calcul				tion	20.00
F						20.00
		Next	E t	Gouth		0754.014
	C00	STEADY-				
9	WCo	STATE WALL				
4	WCt	14 547671	5.196771	5.591365	5.107119	R-value:
Q	Dtu Concumption	14.347071				20.64
H	Dia Consumption	14,547,071				STEADY-
2	HEAT	STATE WALL				
	WCh	3 708222	3 572308	3 333001	3 576626	U-value:
Si I	WCt	14 191148	5.572500	5.555771	5.570020	
V	Btu Consumption	14.191.148	Note I: Btu's consumed		equals	0.05
\geq		1.000.000				
\geq	TOTAL ESTIMA	WALL HEAT				
6	WCt	28.739	Wall Crite	Wall Criteria results in a zero		
Ц	Btu Consumption	28,738,819	value for	1.00		
		1.00				
						1
enne enn	ERMAL MASS, ANAL	TICAL COMP.	ARISON RESU	LTS IN THE		00.01
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